The effects on seismic waves of interconnected nearly aligned cracks

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SUMMARY

Transfer of fluid between connected cracks may occur during the passage of seismic waves. Such fluid flow can be modelled using an extension of effective medium theory (Hudson et al. 1996) and is effected via non-compliant pores. The flow is governed by a parameter $\tau$ representing the relaxation time of pressure equalization between cracks. However, if the cracks are fully aligned and have the same aspect ratio, the theory produces the unexpected result that, at low frequencies, the cracks are effectively isolated and at high frequencies they are fully drained. The artificial restriction of the model to perfectly aligned cracks of identical aspect ratio is seen to be the cause of this result. By reworking the model to allow the crack orientation and aspect ratios to vary, we see that a more realistic model has the usual properties in which the cracks are isolated at high frequencies and undrained at low frequencies. We have chosen the distributions of aspect ratios to be in agreement with observation (Hay et al. 1988). Thomsen’s parameters (Thomsen 1986) and the attenuation coefficients are seen to be frequency-dependent via the non-dimensional parameter $\nu t$.  

Key words: anisotropy, cracks, permeability, porosity.

1 INTRODUCTION

Cracking originates in rocks from a number of geological processes, of which thermal gradients and tectonic stress are particularly important. The resulting fracture network will depend upon both the mineralogy and grain orientation within the rock. Experiments on thermally induced cracking (Fredrich & Wong 1986; Hadley 1976; Homand-Etienne & Houpert 1989) and stress-induced cracking (Montoto et al. 1995; Tapponnier & Brace 1976; Wong 1982) suggest that the former process produces a fairly isotropic distribution of predominantly intergranular cracks, while the latter produces a strongly anisotropic distribution of intragranular and transgranular cracks, with the majority of cracks oriented parallel to the direction of maximum principal stress (David et al. 1999; Menéndez et al. 1999).

Effective medium theories giving expressions for the overall mechanical properties (in particular, the wave speeds) of materials with cracks are now well established. Among the best known are the self-consistent method (O’Connell & Budiansky 1974), the method of smoothing (Hudson 1980) and the differential method (Nishizawa 1982). In all such theories it is necessary to calculate the response of a single crack in an unbounded homogeneous matrix. Since all the methods involve extensive averaging, the cracks are represented for this purpose by a ‘mean crack’, usually taken to be circular. The cracks may be aligned, partially aligned or randomly oriented (Hudson 1986), they may be filled with gas (dry), liquid or a weak solid (Hudson 1981) and they may be connected through the porosity of the matrix rock (Hudson et al. 1996; O’Connell & Budiansky 1977). In the latter case, fluid is able to flow between cracks that, because of their difference in orientation, say, have been distorted differently by an imposed stress field. We follow the analysis of Hudson et al. (1996) here and it should be borne in mind that the theory developed here is valid only to first order in the number density of the cracks. Although Hudson et al. (1996) and Pointer et al. (2000) imply that the extension to second order in the number density is straightforward, it has not been established that this is the case and we restrict ourselves to a first-order theory here.

In their paper, Hudson et al. (1996) derived a rather unexpected result for aligned connected cracks. This was that, in high-frequency wave propagation, the cracks behave as if they are completely drained (dry) and, at low frequencies, as if they are isolated without connections. Although apparently running against physical intuition, this result is explained by the fact that because the cracks are fully aligned, the pressure gradient driving fluid from one crack to another varies on the scale of a wavelength, inversely proportional to the frequency $\omega$. Thus, as the frequency tends to zero, the diffusion is less and less effective, with the opposite effect as $\omega \rightarrow \infty$. 

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Hudson et al. (1996) derived their results for aligned cracks by a method that ignores local crack-to-crack flow since it was assumed that because the cracks all have the same orientation, it would be unimportant. However, if the formulae for non-aligned cracks are specialized to cracks with a single orientation, the result differs from the above in the addition of one term that becomes important at high frequencies. The incorporation of crack-to-crack flow shows that it cannot be neglected when the frequency is sufficiently high that the wavelength approaches the size of the intercrack spacing. We compare the two results here and show that, with the more complete theory, fully aligned cracks behave as if isolated at very low frequencies for the reasons given above.

As well as depending on the assumption that the cracks are fully aligned, these results also rely on the fact that the cracks were assumed all to have the same aspect ratio. Relaxing either of these two assumptions leads to local fluid flow between neighbouring cracks that have been distorted in different ways by the incoming wave because of their different orientations or aspect ratios or both. In this paper we analyse the effect of allowing small variations in alignment and aspect ratio and find that the behaviour of the material is that of undrained cracks at low frequencies, in accordance with physical expectation. We show, graphically, how the material behaves when the cracks are nearly aligned and when they all have nearly the same aspect ratio.

2 BACKGROUND

The method of smoothing developed by Keller (1964) has been applied by Hudson (1980, 1981, 1986) to determine expressions for the effective elastic parameters \( c \) of a cracked material, to first order in crack density \( \varepsilon = \langle \varepsilon \rangle \), where \( \varepsilon = N/V \), \( N \) is the number of cracks, \( V \) is the material volume, \( a \) is the crack radius and the operator \( \langle \cdot \rangle \) denotes the mean value, such that

\[
e = e^0 + \epsilon e^1 + \epsilon \langle \epsilon^2 \rangle ,
\]

where \( e^0 \) is the elastic tensor for the assumed isotropic, porous matrix material,

\[
e_{ij}^0 = \lambda \delta_{ij} \delta_{kl} + \mu (\delta_{ij} \delta_{kl} + \delta_{il} \delta_{kj}) ,
\]

where \( \lambda \) and \( \mu \) are the Lamé constants of the material; \( e^i \) accounts for scattering off individual cracks.

Determination of \( e^i \) depends upon the orientations of the cracks and the nature of the crack infill. Expressions for \( e^i \) under varying conditions for isolated cracks can be found in Hudson (1980, 1981, 1986). For aligned isolated cracks of identical aspect ratio, with normals lying in the \( x_3 \)-direction, these are of the form

\[
e_{ij}^1 = -\frac{1}{\mu} \epsilon \rho_{ij} e_{ij}^0 \hat{u}_{ki} ,
\]

where the nature of the crack infill is reflected in the diagonal matrix \( \{ \hat{u}_{ij} \} \), where \( \hat{u}_{11} = \hat{u}_{22} \), due to the assumed symmetry of each crack. The resulting effective medium is vertically transversely isotropic.

3 THEORY

The model of connected cracks proposed by Hudson et al. (1996) for the transfer of fluid between cracks by non-compliant pores (seismically transparent pathways) (see Figs 1a and b) makes the assumptions that the distortion of the pores is negligible compared with that of the cracks during the passage of a wave and that the pore porosity is low, so that we neglect compression of the pore fluid.

The population of cracks is divided into families of parallel cracks with identical aspect ratio and identical radius, labelled \( n = 1, 2, \ldots \). Hudson et al. (1996) give a first-order expression for the porosity of the \( n \)th set of cracks,

\[
\phi_n = \phi_n^0 + \phi_n^1 ; \langle \sigma^0 + p_n^0 \rangle = \frac{\phi_n^0 \rho_n^0}{\kappa} ,
\]

where \( \kappa = \lambda + 2\mu/3 \) is the bulk modulus of the matrix material, \( \phi_n^0 \) and \( \phi_n^1 \) are the stress-free porosity and the first-order dependence on stress, respectively, for the \( n \)th set of cracks, \( \sigma^0 \) is the imposed static stress field and \( p_n^0 \) is the fluid pressure in the \( n \)th set of cracks.

![Figure 1.](image-url)
The relation proposed by Hudson et al. (1996) for the wave flow out of the nth set of cracks, derived in Appendix A, is

$$\frac{\partial (\rho_0 \phi_n)}{\partial t} = -\frac{\phi_0 \rho_0}{\kappa_t} (p_n - p_t),$$

(5)

where $\rho_0$ is the fluid density in the nth set of cracks, $\rho_0$ is the unstrained density, $\kappa_t$ is the bulk modulus of the fluid, $p_t$ is the average (local) pressure in the fluid and $t$ is a relaxation parameter. Estimations of the value of $t$ are made by Hudson et al. (1996) and O’Connell & Budiansky (1977). This gives us the relationship between the fluid pressure, $p_n$, in the nth set of cracks, the average fluid pressure and the imposed static stress,

$$p_n = \left( p_t + i\alpha \gamma_n \right) \left( 1 - i\alpha \gamma_n \right),$$

(6)

with

$$\gamma_n = 1 - \frac{\kappa_t}{\kappa} + \frac{\kappa_t (\phi_1)}{\phi_0} \gamma_n,$$

(7)

where we have used the relationship between the fluid pressure and density,

$$\rho_0 - 1 = \frac{p_n}{\kappa},$$

(8)

and have assumed a plane wave solution to the equations of motion of the form $u = e^{i(k \cdot x - \omega t)}$, so that the operators $\partial \partial t$ and $\partial \partial x$ are replaced by the factors $ik$ and $-i\omega$ respectively. This is the opposite convention to that used by Hudson et al. (1996).

From Hudson et al. (1996), conservation of mass and D’arcy’s law yield an evolution equation for the total mass concentration of fluid, $m_t$,

$$\frac{\partial m_t}{\partial t} = \nabla \cdot \left( \rho_t K' \nabla p_t \right),$$

(9)

with $K'$ the permeability tensor of the matrix, including cracks,—this will be anisotropic, although Hudson et al. (1996) assumed an isotropic permeability; $m_t$ is given by

$$m_t = \sum \rho_n \phi_n,$$

(10)

where $\rho_n$ is the average fluid density, $\eta_t$ is the fluid viscosity, and $p_t$ and $\rho_t$ obey the same relation as $p_n$ and $\rho_n$ in eq. (8).

Let us assume that $K'$ is spatially constant. Substituting eqs (4), (6) and (8) into eq. (10) and using eq. (9) we gain, to first order in $p_t/k_t$ and $\phi_1/\phi_0$, where $\phi_1$ is the average stress-free porosity of the cracks,

$$p_t = \left( 1 - \frac{\kappa_t}{\kappa} \right) \sum \frac{\phi_0}{1 - i\alpha \gamma_n} + \kappa_t \sum \frac{\phi_1}{1 - i\alpha \gamma_n} + \frac{i\alpha \kappa_t K'_{\phi_1} \kappa_{\phi_1}}{\kappa_t},$$

(11)

where

$$\kappa = \frac{k_2}{k}$$

(12)

is the ratio of the wavenumber in the $x_i$-direction to the total wavenumber, and $v$ is the wave speed; we approximate this to lowest order by using either $v_P$ or $v_S$ corresponding to $P$ or $S$ waves respectively.

Letting the normal to the nth set of cracks be $n^i$, from Hudson et al. (1996) we have

$$\frac{\partial \phi_{\phi_n}}{\partial t} = \frac{2v}{\pi \mu \gamma_n} \phi_{\phi_n},$$

(13)

where $z_n = c_n \alpha_n$ is the aspect ratio of the nth set of cracks and

$$v = \frac{\lambda}{2(\lambda + \mu)}$$

(14)

is Poisson’s ratio of the matrix material. We now have

$$\gamma_n = 1 - \frac{2\kappa_t (1 - v)}{\pi \mu \gamma_n} \phi_{\phi_n} + \left( \phi_{\phi_n} \gamma_n \right),$$

(15)

Substituting eq. (13) into eq. (11) yields an expression for $p_t$ and hence by eq. (6) an expression for $p_n$ in terms of $\phi_1$. Thus, from eq. (4), the relative change in porosity becomes

$$\phi_n - \phi_{\phi_n} = \frac{\phi_{\phi_n}}{\phi_0} = \frac{2(1 - v)}{\pi \mu \gamma_n} \left( \phi_{\phi_n} \gamma_n + \phi_{\phi_n} \gamma_n \right) - \gamma_n = 1 - \frac{2\kappa_t (1 - v)}{\pi \mu \gamma_n},$$

(16)

As in Hudson et al. (1996), we write this as

$$\frac{3}{4\pi \mu \gamma_n} N_{\phi_0}^\phi,$$

(17)

thus defining $\{N_n^\phi\}$, the crack opening parameters for the nth set of cracks. This is a modified version of the corresponding result derived in Hudson et al. (1996) that allows for variable aspect ratio.

The analysis of Hudson et al. (1996) now proceeds to show that the perturbation $\epsilon_{ij}$ in the elastic parameters is given by

$$\epsilon_{ij} = \sum \frac{\epsilon_{ij}}{\mu} = \sum \sum \frac{\epsilon_{ij}}{\mu} n_0 n_0 + \sum \sum \frac{\epsilon_{ij}}{\mu} n_0 n_0,$$

(18)

where $\epsilon_{ij}$ is the crack density of the nth set of cracks; that is, $\epsilon_{ij} = \omega_n \gamma_n$, where $\omega_n$ is the number density and $\gamma_n$ is the radius of the nth set of cracks.

$\{N_{\phi_0}^\phi\}$ is the rotation matrix from the background axes to axes fixed in the crack with normal in the $x_3$-direction, so that

$$l_{\phi_0} = n^3, \quad l_{\phi_0}^\phi = \delta_{33},$$

(19)

and we have adopted the opposite convention for the definition of $\{l_{\phi_0}^\phi\}$ to Hudson (1986), Hudson et al. (1996) and Pointer et al. (2000). We note that Hudson et al. (1996) incorrectly stated their choice of the sense of the rotation $\{l_{\phi_0}^\phi\}$. The values of $\{N_{\phi_0}^\phi\}$ in eq. (18) are to be calculated for cracks with normals in

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the \(x_3\)-direction, \(N_0^3\) is given by Hudson (1981) for a weak viscous material infill with effective rigidity \(-\eta_{1i}\) as

\[
\ddot{W}_{11}^m = \frac{16}{3} \frac{1 - v}{(1 + M_n)}.
\]

where

\[
M_n = -\frac{4J_1}{\pi} \frac{1 - v}{\mu} \eta_{1i}.
\]

Inserting eq. (20) into eq. (18), we finally arrive at an expression for the first-order correction to the elastic constants,

\[
\varepsilon_k^1 = -\sum_n \frac{f_n}{\eta} \sum_{i,j,k,l} \frac{f_{i,j,k,l}}{\eta_{i,j,k,l}} \left( \delta_{13} \delta_{13} \delta_{13} (1 - v) - \frac{1 - i\sigma \eta_{1i}}{1 - i\sigma \eta_{1i}} \right)
\]

\[
\times \left[ \delta_{13} \delta_{13} + \delta_{23} \delta_{23} \right] \dot{W}_{11}^m + \frac{8}{3} (1 - v) \sum_n \frac{f_n}{\eta} \sum_{i,j,k,l} \frac{f_{i,j,k,l}}{\eta_{i,j,k,l}} \left( \delta_{13} \delta_{13} \delta_{13} (1 - v) - \frac{1 - i\sigma \eta_{1i}}{1 - i\sigma \eta_{1i}} \right)
\]

\[
\times \sum_m \frac{\epsilon_m}{1 - i\sigma \eta_{1i}} \left( \sum_n \frac{f_n}{\eta} \sum_{i,j,k,l} \frac{f_{i,j,k,l}}{\eta_{i,j,k,l}} \left( \delta_{13} \delta_{13} \delta_{13} (1 - v) - \frac{1 - i\sigma \eta_{1i}}{1 - i\sigma \eta_{1i}} \right) \right)^{-1}.
\]

\[
(23)
\]

4 HIGH- AND LOW-FREQUENCY LIMITS

The behaviour of eq. (23) at high frequency is given by

\[
\varepsilon_k^1 = -\sum_n \frac{f_n}{\eta} \sum_{i,j,k,l} \frac{f_{i,j,k,l}}{\eta_{i,j,k,l}} \left( \delta_{13} \delta_{13} \delta_{13} (1 - v) - \frac{1 - i\sigma \eta_{1i}}{1 - i\sigma \eta_{1i}} \right)
\]

\[
\times \left[ \delta_{13} \delta_{13} + \delta_{23} \delta_{23} \right] \dot{W}_{11}^m + \frac{8}{3} (1 - v) \sum_n \frac{f_n}{\eta} \sum_{i,j,k,l} \frac{f_{i,j,k,l}}{\eta_{i,j,k,l}} \left( \delta_{13} \delta_{13} \delta_{13} (1 - v) - \frac{1 - i\sigma \eta_{1i}}{1 - i\sigma \eta_{1i}} \right)
\]

\[
\times \sum_m \frac{\epsilon_m}{1 - i\sigma \eta_{1i}} \left( \sum_n \frac{f_n}{\eta} \sum_{i,j,k,l} \frac{f_{i,j,k,l}}{\eta_{i,j,k,l}} \left( \delta_{13} \delta_{13} \delta_{13} (1 - v) - \frac{1 - i\sigma \eta_{1i}}{1 - i\sigma \eta_{1i}} \right) \right)^{-1}.
\]

\[
(24)
\]

which corresponds to the result for isolated cracks filled with a fluid with \(\omega \eta_{1i} \ll \kappa \ll \kappa\) (Hudson 1981); that is, a fluid such that its effective rigidity is small in relation to its bulk modulus, which in turn is negligible in comparison with the bulk modulus of the material. The low-frequency limit of eq. (23) is

\[
\varepsilon_k^1 = \frac{8}{3} (1 - v) \sum_n \frac{f_n}{\eta} \sum_{i,j,k,l} \frac{f_{i,j,k,l}}{\eta_{i,j,k,l}} \left( \delta_{13} \delta_{13} \delta_{13} (1 - v) - \frac{1 - i\sigma \eta_{1i}}{1 - i\sigma \eta_{1i}} \right)
\]

\[
\times \left[ \delta_{13} \delta_{13} + \delta_{23} \delta_{23} \right] \dot{W}_{11}^m + \frac{8}{3} (1 - v) \sum_n \frac{f_n}{\eta} \sum_{i,j,k,l} \frac{f_{i,j,k,l}}{\eta_{i,j,k,l}} \left( \delta_{13} \delta_{13} \delta_{13} (1 - v) - \frac{1 - i\sigma \eta_{1i}}{1 - i\sigma \eta_{1i}} \right)
\]

\[
\times \sum_m \frac{\epsilon_m}{1 - i\sigma \eta_{1i}} \left( \sum_n \frac{f_n}{\eta} \sum_{i,j,k,l} \frac{f_{i,j,k,l}}{\eta_{i,j,k,l}} \left( \delta_{13} \delta_{13} \delta_{13} (1 - v) - \frac{1 - i\sigma \eta_{1i}}{1 - i\sigma \eta_{1i}} \right) \right)^{-1}.
\]

\[
(25)
\]
therefore eq. (34) becomes
\[
s_{jk} - s_{jk}^0 = -\frac{8}{3} \left(1 - \nu\right) \frac{2\kappa_1(1 - \nu)}{\pi \mu \gamma_0 \gamma} \sum_n \frac{\kappa_n}{\mu} n_n^j n_n^k \sum_m \frac{\kappa_m}{\mu} n_m^j n_m^k ,
\]
(37)
where
\[
\gamma_0 = 1 - \frac{\kappa_1}{\kappa} + \frac{2\kappa_1(1 - \nu)}{\pi \mu \gamma_0} .
\]
(38)

We note that \(\Sigma_m \kappa_m = \kappa\) and \(\Sigma_m \kappa_m \xi_m = \xi \) provided that we assume that \(\xi\) and \(\rho\) are independently distributed parameters; then, from the definition of \(\gamma_m\) (eq. 15), \(\Sigma_m \kappa_m \xi_m \xi_m = \xi \) and hence, from eq. (30),
\[
\epsilon \| k \|^b_{jk} = -\frac{8}{3} \left(1 - \nu\right) \frac{\mu}{\pi \gamma_0 \gamma} \sum_n \frac{\kappa_n}{\mu} n_n^j n_n^k \sum_m \frac{\kappa_m}{\mu} n_m^j n_m^k \xi (\gamma_n - 1) \sum_m \frac{\kappa_m}{\mu} n_m^j n_m^k .
\]
(39)

We can neglect the term \(\kappa_1 \rho\) in \(\gamma_0\) on the assumption that the maximum value of the aspect ratio, \(\gamma_{\text{max}}\), satisfies the condition
\[
\gamma_{\text{max}} \ll \frac{4(1 - \nu^2)}{3(1 - 2\nu)} ,
\]
(40)
which is consistent with our restriction to small aspect ratios provided that \(\gamma \neq 1\); then the term \(\gamma (\gamma_n - 1)\) in eq. (39) is independent of \(n\), and eq. (39) reduces to the right-hand side of eq. (37) exactly, so the undrained parameters are given by
\[
s_{jk} = s_{jk}^0 - \frac{8}{3} \left(1 - \nu\right) \frac{2\kappa_1(1 - \nu)}{\pi \mu \gamma_0 \gamma} \sum_n \frac{\kappa_n}{\mu} n_n^j n_n^k \sum_m \frac{\kappa_m}{\mu} n_m^j n_m^k .
\]
(41)

This is identical to eq. (30) for the low-frequency limit for connected cracks, showing that, at low frequencies, connected cracks respond at each point in exactly the same way as the same material under static, undrained conditions.

5 CONTINUOUS LIMIT

Having developed the theory from a discrete perspective, we shall henceforth assume a continuous limit: \(\Sigma_n F(\theta)\) in eq. (23) is replaced by
\[
\int_0^\infty \int_0^\infty \int_0^\infty \int_0^{2\pi} F(\phi, \theta, a, \rho) f_\phi f_\theta f_a f_\rho \sin \theta d\phi d\theta d\rho d\alpha
\]
(42)
for any function \(F\), where \(f_\phi, f_\theta, f_a\) and \(f_\rho\) are the probability distribution functions of the random variables \(\phi, \theta, a\) and \(\rho\) (defined by polar angles \(\phi\) and \(\theta\)) respectively. We shall assume that these distributions are independent of one another, for the purpose of separately assessing their effects on seismic anisotropy. More realistically perhaps, one would expect aspect ratio to depend upon orientation, with cracks parallel to the direction of maximum principal stress having a larger mean aspect ratio than those perpendicular to it. Gibson & Toksöz (1990) developed a model of a probability density function for crack orientation with an aspect ratio distribution included. Their results from the inversion of velocity measurements are generally good, although there is an implied non-uniqueness of inversion.

Prior to the exposure to stress, a rock will have a generally isotropic background distribution of cracks (David et al. 1999). Stress will induce further cracking, which will be of an anisotropic nature (Menéndez et al. 1999), and thus a more accurate description of crack distributions within a rock may be obtained by representing the crack distribution as the sum of an isotropic and an anisotropic part.

For a given aspect ratio, the crack radius \(a_n\) only appears within the term \(\epsilon_n\) in eq. (23), so that in the continuous limit it occurs in the form of \(\langle a_n^3 \rangle\) only, and thus \(\epsilon_n\) may be replaced everywhere by \(\epsilon\).

6 ALIGNED CRACKS

If we take the limit in which the cracks are fully aligned and of identical aspect ratio, we find that \(\epsilon^1\) is given by eq. (3), with
\[
\bar{\epsilon}_{11} = \frac{16}{3} \left(1 - \frac{v}{v_t}\right) \left(1 + M_{\text{align}}\right),
\]
(43)
\[
\bar{\epsilon}_{33} = \frac{8}{3} \left(1 - \nu\right) / \left(1 + K_{\text{align}}\right)
\]
(44)
and
\[
M_{\text{align}} = -\frac{4}{\pi} \frac{1 - v}{2 - v} \nu \eta \nu_{\text{intr}} P_{m} ,
\]
(45)
\[
K_{\text{align}} = \frac{2\kappa_1(1 - \nu)}{\pi \mu \gamma_0 \gamma} \left(1 + \frac{\nu \eta T k^0 \nu}{\nu \nu_{\text{intr}} k_{k}^0}\right)^{-1} ,
\]
(46)
where
\[
\nu_{\text{intr}} = \frac{\eta}{\mu \gamma^2} ,
\]
(47)
and
\[
\nu^b = \frac{3\kappa_1 K_{k}^0 \nu_{\text{intr}} k_{k}^0}{4\pi \mu \gamma^2 \nu_{\text{intr}}} ,
\]
(48)
The quantity \(\nu \nu_{\text{intr}} P_{m}\) is identical to the intracrack viscosity parameter \(P_{m}\) of Pointer et al. (2000), who estimated that, with the fluid properties of oil or water, its effect is negligible for seismological applications for both aligned and randomly oriented cracks.

We have written the expressions in eqs (45) and (46) in terms of \(\nu_{\text{intr}}\), which is the short-range diffusion parameter \(P_{m}\) of Pointer et al. (2000) and the quantity \(\nu_{\text{intr}} P^b\) is \(3/4\pi\) times the long-range diffusion parameter \(P_{m}\) of Pointer et al. (2000). Apart from the presence of an additional term—the \(\kappa_1\nu/k_{k}\) term, neglected by Hudson et al. (1996)—this result is identical to the aligned limit of the expression derived for non-aligned cracks by Hudson et al. (1996). Both of these expressions for aligned cracks with identical aspect ratio differ from that given by Hudson et al. (1996) is
\[
K_{\text{align}} = \frac{2\kappa_1(1 - \nu)}{\pi \mu \gamma_0 \gamma} \left(1 - \frac{\nu \eta T k^0}{\nu \nu_{\text{intr}} k_{k}^0}\right) ,
\]
(49)
which ignores the term \((\nu \nu_{\text{intr}} P_{m})^b\) and uses the opposite sign convention on the temporal derivative. This difference arises as a result of the failure of the aligned cracks result (Hudson et al. 1996) to account for any local fluid flow (note that \(\nu_{\text{intr}} P^b\) is independent of \(\tau\)).
We see from eq. (46) that in either of the limits \( \omega \tau \rightarrow 0 \) or \( \omega \tau \rightarrow \infty \),
\[ K^{\text{simple}} = \frac{2\kappa_i (1 - v)}{\pi \mu_\varphi} - \frac{\kappa_i}{k}, \tag{50} \]
which is the result for isolated cracks filled with a fluid with \( \omega \tau \approx \ll \kappa_i / \kappa \) (Hudson 1981). The inclusion of local crack-to-crack flow gives the expected result at high frequencies, but at very low frequencies the cracks still act as if isolated for the reasons given earlier.

7 VARIABLE ASPECT RATIO

To begin with, we assume that the cracks are fully aligned, hence
\[ f = (\theta, \phi, \phi_0) = \delta(\theta - \theta_0)\delta(\phi - \phi_0) / \sin \theta, \tag{51} \]
and consider the effects of variable aspect ratio only. Let us further assume that \( \theta_0 = 0 \), so that all the cracks now have normals in the \( x \)-direction. Eq. (23) now takes a form identical to that of eq. (3),
\[ \epsilon_{ij}^{(1)} = \frac{1}{\mu} \epsilon_{ijk} \epsilon_{jkl}, \tag{52} \]
where \( \epsilon_{ijk} \) is a diagonal matrix with
\[ \epsilon_{11} = \epsilon_{22} = \frac{16}{3} \left( 1 + M^2 \right), \tag{53} \]
\[ \epsilon_{33} = \frac{8}{3} \left( 1 - v \right) F_1 / (1 + K'), \tag{54} \]
and
\[ M^2 = 4i \left( 1 - v \right) \omega \tau M^2 E(m) \left[ 1 + 4i \left( 1 - v \right) \omega \tau M^2 E(m) \right]^{-1}, \tag{55} \]
\[ K' = (\gamma_0 - 1) \times \left[ 1 + \frac{1 - i \gamma_0}{F_1 - (F_2 - F_1) \gamma_0 (1 - \gamma_0) / (1 - \gamma_0 - i \gamma_0)} \right]^{-1}. \tag{56} \]

We have defined here two functions that depend upon the probability distribution function of \( x \),
\[ F_1 = \frac{1 - i \gamma_0}{\gamma_0} \int_0^\infty \frac{dx}{1 - i \gamma_0} \left( \frac{1 - i \gamma_0}{1 - i \gamma_0 (1 - \gamma_0 / k)/k} \right)^2 \times \left[ 1 - i \gamma_0 (1 - \gamma_0 / k) + i \gamma_0 (\gamma_0 - 1 + \gamma_0 / k) E(k) \right] \tag{57} \]
and
\[ F_2 = \frac{1 - i \gamma_0}{\gamma_0} \int_0^\infty \frac{dx}{1 - i \gamma_0} \left( \frac{1 - i \gamma_0}{1 - i \gamma_0 (1 - \gamma_0 / k)/k} \right)^2 \times \left[ -\gamma_0 (\gamma_0 - 1 + \gamma_0 / k)^2 E(k) \right] \tag{58} \]
where
\[ E(y) = y_0 \left( \frac{1}{2 + y_0} \right)^2, \tag{59} \]
and the parameters of the distribution are chosen such that \( \langle x \rangle = \delta_0 \). Finally,
\[ k = \frac{2i (1 - v)}{\pi \mu_\varphi} \frac{1 - i \tau (1 - \kappa_i / k)}{1 - i \tau (1 - \kappa_i / k)} \tag{60} \]
and
\[ m = \frac{-4i \left( 1 - v \right) \omega \tau M^2}{\pi^2 - v}. \tag{61} \]

We can generalize this result to the case of arbitrary values of \( \theta_0 \) and \( \phi_0 \), letting the normal to the cracks be \( n = \sin \phi_0 \cos \theta_0, \sin \phi_0 \sin \theta_0 \cos \phi_0, \sin \theta_0 \sin \phi_0 \cos \theta_0 \),
\[ c_{ij}^{(1)} = \frac{1}{\mu} \epsilon_{ijk} \epsilon_{jkl} \tilde{U}_{ki}, \tag{62} \]
where \( \tilde{U}_{ij} \) is just the rotation of \( \tilde{\epsilon}_{ij} \) to the new axes and is given by
\[ \tilde{U}_{ij} = \left( \delta_{ij} - n_j n_i \right) \tilde{U}_{11} + n_j n_i \tilde{U}_{33} \tag{63} \]
with \( \tilde{U}_{11} \) and \( \tilde{U}_{33} \) given as above (eqs 53 and 54).

7.1 Modelling the distribution

Our theory restricts us to consider \( \alpha \ll 1 \) only, so we look for distributions with a finite range and a small mean. For this we have chosen a generalized form of the Beta distribution (e.g. Ross 1989), Beta\((\alpha, \beta)\), with a probability density function (pdf)
\[ f_\alpha(\alpha, \beta, \beta, q) = \frac{1}{\mu B(\alpha, \beta)} \frac{(\gamma - 1 - \gamma_0)^{\alpha - 1}}{\gamma_0 - 1 + \gamma_0 q^\alpha} \tag{64} \]
for \( 0 \leq \gamma \leq \mu \), with \( p, q > 0 \),
and \( B(x, y) \) is the Beta function (e.g. Carrier et al. 1983). The three parameters \( p, q \) and \( u \) allow us considerable flexibility with our model and in particular we may choose them such that the pdf closely resembles observational results (Hay et al. 1988).

We wish to fit the parameters of the distribution such that
\[ \langle x \rangle = \delta_0 \tag{65} \]
\[ \text{Var}(x) = \langle x^2 \rangle - \langle x \rangle^2 = (\delta_0)^2 \tag{66} \]
for some \( \delta > 0 \). Thus we choose \( p \) and \( q \) such that
\[ p = \frac{u - \gamma_0 - \gamma_0 \delta^2}{\gamma_0^2}, \tag{67} \]
\[ q = \frac{u - \gamma_0 - \gamma_0 \delta^2}{\gamma_0^2} \tag{68} \]
Our choice of \( \delta \) will dictate the spread of the distribution and \( u = u_{\text{max}} \), the maximum value of \( x \) that can be achieved.

Choosing \( u = 0.2 \), \( \gamma_0 = 0.00837 \) and \( \delta = 0.703 \) ensures that our probability density function resembles the results of Hay et al. (1988) (see Fig. 2) based upon a truncation of the data provided in Hay (1988), where the larger aspect ratio values have been ignored. For \( x \) greater than some critical value much less than \( u \), the pdf is effectively zero; it is not surprising, therefore, that variations in \( u \) have a negligible effect upon the...
values of the elastic constants—while there is a very small observable difference between the Beta distribution with \(a=0.2\) and 0.5 (Fig. 2), there is no discernible difference between the resulting components of the stiffnesses (eq. 52)—so we replace eq. (64) with

\[
\begin{align*}
\hat{e}_s(x|\alpha, \delta) &= \lim_{\alpha, \delta \to 0} \hat{e}_s(x|\mu, \sigma) \\
&= \frac{(\alpha \delta)^{-1/\delta}}{\Gamma(1/\delta)} x^{1/\delta-1} e^{-x/\alpha \delta^\delta}, \quad \text{for } 0 \leq x,
\end{align*}
\tag{67}
\]

which is a Gamma\((1/\delta, 1/\alpha \delta)\) distribution (Ross 1989), with \(\Gamma(z)\) the Gamma function (Carrier et al. 1983). Graphically, this looks almost identical to the Beta distribution with \(a=0.5\) (Fig. 2). With this choice of distribution, we have

\[
E(y) = \frac{1/\delta}{\Gamma(1/\delta)} \int_0^{\infty} \frac{x^{1/\delta-1} e^{-x}}{x+y/\delta^\delta} \, dx.
\tag{68}
\]

7.2 Results

We start by choosing the parameters of the Gamma distribution such that it closely follows the measurements of Hay et al. (1988); thus \(\alpha_0=0.00837\) and \(\delta=0.703\). Furthermore, we shall use \(\varepsilon=0.02\), \(\nu=3.5 \times 10^7\) m s\(^{-1}\), \(\nu_x=2.0 \times 10^4\) m s\(^{-1}\) and \(\rho=2.2 \times 10^6\) kg m\(^{-3}\) (average values that could correspond to a large number of possible matrix materials), \(\kappa_t=2.25 \times 10^6\) Pa and \(\eta_1=10^{-3}\) Pa s (for water), thus \(\nu=0.258\) and \(\kappa_t/\kappa=0.148\). We shall, for simplicity, assume that \(\{K_{pq}\}=K'\delta_{pq}\) and use \(K'=10^5\) mD \((\approx 10^{-12} \mu\text{m})\), so that only the parameter \(\varepsilon\) remains unknown in the expressions for \(P^m\) and \(P^s\) (eqs 47 and 48 respectively).

We start by considering the variation of Thomsen’s parameters (see Appendix B) with the non-dimensional frequency \(\omega T\) and the constants \(P^s\) and \(P^m\). From the definitions (eqs B1, B2 and B3),

\[
\varepsilon_T = \frac{4\varepsilon}{1-2\nu} \mathcal{R}(\mathbf{\hat{H}}_{13}),
\tag{69}
\]

\[
\delta_T = \varepsilon \left[ \frac{2\mathcal{R}(\mathbf{\hat{H}}_{13})}{1-2\nu} - \frac{1}{1-\nu} \mathcal{R}(\mathbf{\hat{H}}_{11}) \right]^{(a)}
\tag{70}
\]

and

\[
\gamma_T = \frac{\varepsilon}{2} \mathcal{R}(\mathbf{\hat{H}}_{11})
\tag{71}
\]

to first order in crack density \(\varepsilon\). Thus \(\varepsilon_T\) (a measure of the \(P\)-wave anisotropy) is independent of \(P^m\) and, from Fig. 3(a), is described by a bell-shaped curve for lower values of \(P^s\) that develops a flat top for higher values, while \(\gamma_T\) (a measure of the \(SH\)-wave anisotropy) is independent of \(P^s\) and is described by a monotonically decreasing curve (see Fig. 3b); \(\delta_T\) depends upon both \(P^s\) and \(P^m\).

We see from Fig. 3(a) that increasing \(P^s\) results in an increase in the magnitude of the peak of \(\varepsilon_T\) up to a maximum reached at \(P^s \approx 10^6\) and a decrease in the value of \(\varepsilon_T\) at which the peak occurs, at approximately \(\omega T = (P^s)^{-1/2}\)—thus we see that the term \((\omega T)^{1/2}\) \(P^m\) dominates eq. (56). Increasing \(P^s\) still further does not change the peak value of \(\varepsilon_T\), but broadens the range of \(\omega T\) within which \(\varepsilon_T\) is non-negligible.

From Fig. 3(b) it can be seen that an order of magnitude increase in the value of \(P^m\) results in an order of magnitude decrease in the value of \(\varepsilon_T\) at which a transition is made from

\[
\begin{align*}
\gamma_T &= \frac{\varepsilon}{2} \mathcal{R}(\mathbf{\hat{H}}_{11})
\tag{71}
\end{align*}
\]
the maximum to the minimum values of $\gamma_T$ (as $\omega_T \to \infty$, $E_{\text{iso}} \to 0$) such that $M \to \infty$ and thus $\Psi_{11} \to 0$ with the transition occurring over a range $[0.1 (P^p)^{-1}, 10 (P^p)^{-1}]$ of $\omega_T$. We now consider the effect upon Thomsen’s parameters of the distribution parameter $\delta$ and the crack density $\varepsilon$. In Fig. 4(a) we consider the effect of $\delta$ and $\varepsilon$ upon $\varepsilon_T$, for $P^p = 10^4$.

We see that a decrease in the variance of the distribution increases the value of $\varepsilon_T$ at its peak—that is, it increases the degree of anisotropy, as we would expect. The greatest value of $\varepsilon_T$ is obtained for $\delta = 0$, where all the cracks have the same aspect ratio. Although this case corresponds to an anomalous result for the elastic moduli at low frequencies, we see that the behaviour of $\varepsilon_T$ in the limit $\delta \to 0$ is not remarkable. Away from the peak value, little change is seen in the value of $\varepsilon_T$ when $\delta$ is varied. Furthermore, we note that an increase in the crack density also serves to increase the peak value of $\varepsilon_T$—thus decreasing the variance from 0.703 to 0 (the aligned case) produces a result that is very similar to that achieved by increasing the crack density from 0.2 to 0.0216, and similarly, increasing the variance to 1.0 (an exponential distribution) is seen to be almost equivalent to decreasing the crack density to 0.0182.

So can we distinguish between the effects of the crack density $\varepsilon$ and the variance of the aspect ratio distribution $\delta$? At values of $\omega_T$ away from the peak value of $\varepsilon_T$, a change in $\delta$ will not affect the value of $\varepsilon_T$, whereas an increase or decrease in $\varepsilon$ will cause an increase or decrease, respectively, in $\varepsilon_T$; however, this effect is barely discernible for such small changes in $\varepsilon$ as those discussed above. For larger values of $P^p$, we are more able to distinguish between the two effects (see Fig. 4b), where now $P^p = 10^5$. Only a small change is seen in $\varepsilon_T$ with $\delta$, but a notably different change is seen when adjusting the value of $\varepsilon$.

Fig. 4(c) shows how $\gamma_T$ varies with $\delta$ and $\varepsilon$, for $P^p = 10^5$. We see that a reduction in the variance of the aspect ratio distribution will increase the value of $\gamma_T$ at which the transition from the maximum to minimum values of $\gamma_T$ begins, without affecting the point at which the minimum value is reached. This effect can be distinguished from changes in the value of $\varepsilon$, which clearly increases or decreases the maximum value of $\gamma_T$ with $\omega_T$ as it is increased or decreased respectively.

The attenuation coefficients $Q^{-1}$ for the three waves are defined in eqs (C13), (C14) and (C15); these are dependent upon the incident angle of a wave. For an incident wave parallel to the direction of the crack normals (and thus perpendicular to the cracks), the $x_T$ direction, the change in $Q_{Q^p}$ with frequency is shown in Fig. 5(a) for different values of the parameter $P^p$ and Fig. 5(b) for different values of $\varepsilon$ and $\delta$. For values of $P^p$ smaller than about $10^3$, there is a single peak in the value of $Q_{Q^p}$. For sufficiently large $P^p$ this peak remains at a fixed frequency and amplitude, while a second peak occurs at a frequency that decreases as $P^p$ increases. Comparing Figs 3(a) and 5(a), we see that the frequencies at which the peaks in the attenuation parameter $Q_{Q^p}$ occur coincide with the frequencies of the maximum gradient in the corresponding plot of $\gamma_T$. A change in $\varepsilon$ clearly changes the magnitude of both peaks (see Fig 5b) and a change in $\delta$ produces a larger change in the magnitude of the higher-frequency peak than it does in the lower-frequency peak. Indeed, for larger values of $P^p$, a change in $\delta$ has no effect on the magnitude of the low-frequency peak. Thus, we can always adjust the value of $\varepsilon$ to mimic the effect on the high-frequency peak in $Q_{Q^p}$ of a change in $\delta$, but both peaks cannot be simultaneously matched. The relative heights of the two peaks should be able to give us an indication of the value of $\delta$, assuming that both frequencies are seismically possible. At an incident angle parallel to the cracks, $Q_{Q^p}$ shows a similar variation with the parameters $P^p$, $\varepsilon$ and $\delta$, but is of an order of magnitude smaller (not shown).

Being able to distinguish between the effects of $\delta$ and $\varepsilon$ on $Q_{Q^p}$ is far less likely (see Fig. 6). The frequency at which the peak in $Q_{Q^p}$ occurs coincides with the frequency at which the corresponding plot of $\gamma_T$ has a maximum gradient (see Fig. 3b).
8 VARIABLE ORIENTATION

We shall now consider the effects of allowing the orientation of the crack normals to vary while keeping $x$ constant; thus

$$f_k(x|a_0) = \delta(x - a_0). \quad (72)$$

We find that

$$c^{\hat{y}}_{ij} = -\frac{1}{\mu} c^\phi_{ij} c^0_{ijkl} T_{k\nu s}, \quad (73)$$

where

$$T_{k\nu s} = \left[\delta_{ij} \delta_{kl} + \frac{2}{3} \delta_{k\nu} \delta_{ij} (1 - v) + \frac{1 - \nu}{1 - 2\nu} \Omega_{\delta, ij s}\right] \frac{1 - \nu}{1 - 2\nu} \Omega_{\delta, ij s},$$

$$\Omega_{\delta, ij s} = \int_0^{\pi} \int_0^{\pi} \int_0^{\pi} \int_0^{\pi} \frac{1}{2\pi} \delta(t d\phi d\theta).$$

and

$$\Pi_k = \int_0^{\pi} \int_0^{\pi} \int_0^{\pi} \int_0^{\pi} \frac{1}{2\pi} \delta(t d\phi d\theta).$$

$$\bar{\omega}_{ii} = \frac{16}{3} \frac{1 - \nu}{2 - \nu} \frac{(1 + M)}{\pi},$$

$$M = \frac{4(1 - \nu)}{\pi} \frac{1}{2 - \nu} \nu T^m.$$  \quad (74)

8.1 Modelling the distribution

We shall make the assumption that the crack distribution is rotationally symmetric—that is, the cracks are uniformly distributed with respect to $\phi$—and consider distributions for $n$ that are concentrated around a mean orientation. We use the Watson distribution (Mardia 1972; Fisher et al. 1987), a bipolar distribution, such that

$$f_n = \frac{b(k)}{2\pi} e^{-\frac{1}{2}(\sin \theta \sin \phi \cos \theta + \cos \phi \cos \theta)^2} \quad \text{for}$$

$$0 \leq \theta \leq \pi/2, \quad 0 \leq \phi \leq 2\pi \quad \text{and} \quad k \geq 0,$$  \quad (79)

where

$$b(k) = \frac{1}{\left(\int_0^1 e^{k^2} dt\right)}$$  \quad (80)

and we have restricted the range of $\theta$ to half that given in the original definition of the distribution, to avoid any ambiguity in the definition of crack-normal orientation (as Peacock & Hudson 1990). We shall take $\phi_0 = 0$ so that the mean orientation of the normal, $n^0 = (0, 0, 1)^T$, is along the $x_3$-axis, and the resulting effective medium is vertically transversely isotropic.

The parameter $k$ is a measure of the variance of the distribution,

$$\text{Var}(n) = \left(n - n^0\right)^2 = 2 - 2I_{11},$$  \quad (81)

where the integral $I_{11}$ is defined by eq. (D1). $k = 0$ corresponds to a uniform (isotropic) distribution and as $k \to \infty$, the distribution approaches a delta-like function (eq. 51), so that the cracks are fully aligned. With this distribution, we find that
\( \{ \Omega_{ij} \} \) is diagonal, with
\[
\Pi_{11} = \Pi_{22} = \frac{1}{2} I_{3,0},
\]
\[
\Pi_{33} = I_{1,2}.
\]

To evaluate the components of \( \{ \Omega_{dcr,ax} \} \) we must find \( \{ l_{ij} \} \), given that
\[
l_{1i} = n_i, \quad l_{0j} = \delta_{3j}.
\]

The rotation \( \{ l_{ij} \} \) is given by Fisher et al. (1987) as
\[
\{ l_{ij} \} = \begin{pmatrix}
\cos \psi \cos \phi & -\sin \phi & \sin \psi \\
\cos \psi \sin \phi & \cos \phi & 0 \\
-\sin \psi & 0 & \cos \psi
\end{pmatrix}
\]

where \( \psi \) represents an arbitrary rotation about the \( x_3 \)-axis. \( \{ T_{dcr,ax} \} \) (eq. 74) is independent of the angle \( \psi \), and those elements of \( \{ T_{dcr,ax} \} \) that contribute to \( \{ T_{dcr,ax} \} \) are given in Appendix D.

### 8.2 Results

The effect upon Thomsen’s parameters of the crack orientation distribution is now considered. We examine how they vary with \( \omega_T, P^c, P^m, \varepsilon \) and the distribution parameter \( k \). We use the same values of all of the parameters as with the variable aspect ratio model.

We no longer have such simple expressions for Thomsen’s parameters as eqs (69), (70) and (71), while \( \gamma_T \) remains independent of the parameter \( P^c \), and \( \varepsilon_T \) now depends upon both \( P^c \) and \( P^m \), as does \( \delta_T \), as before. When \( k=0.0 \), the distribution of crack-normal orientations is uniform (i.e. isotropic) and all of Thomsen’s parameters are identically zero. For \( k=10.0 \), the distribution of crack-normal orientations about the mean is given in Fig. 7, and with \( P^m=10^4 \), the variation of \( \varepsilon_T \) with \( \omega_T \) for a range of values of \( P^c \) is shown in Fig. 8(a). We note that Figs 8(a) and 3(a) look very similar; however, it is not now until \( P^c=10^7 \) that \( \varepsilon_T \) reaches its largest peak value. The peak values obtained are less than the corresponding ones in Fig. 3(a).

By choosing a different value of \( P^m \), we would have made only a minimal difference to Fig. 8(a). A smaller value of \( P^m \) would result in a larger value for \( \varepsilon_T \), but only for smaller values of \( P^c \), whereas a larger value of \( P^m \) would reduce \( \varepsilon_T \) for the larger values of \( P^c \)—these effects would be difficult to distinguish from either a larger value of the distribution parameter \( k \) or a more tightly concentrated distribution or an increased crack density \( \varepsilon \).

In Fig. 8(b) we show the variation of \( \gamma_T \) with \( P^m \) (independent of \( P^c \)); compare this with Fig. 3(b). Certainly there is a considerable similarity, as with \( \varepsilon_T \); however, for \( P^m=10^4 \) and higher, the transition from the maximal to minimal values of \( \gamma_T \) occurs over a larger range of \( \omega_T \) than for the variable aspect ratio model; indeed, for \( P^m \) higher than \( 10^4 \), \( \gamma_T \) appears to reach a non-zero minimal value before finally approaching zero at higher values of \( \omega_T \).

For the choice of parameters \( P^c=10^4 \) and \( P^m=10^4 \), the effect on \( \varepsilon_T \) of a change in \( k \) is indistinguishable from a change in \( \varepsilon \), except perhaps at low frequencies. From Fig. 9(a) it is seen that increasing \( k \) to infinity (the fully aligned limit) appears identical to increasing the crack density to \( \varepsilon=0.0242 \), while decreasing \( k \) to 1.0 appears indistinguishable from decreasing \( \varepsilon \) to 0.0034. Altering the value of \( P^c \) or \( P^m \) does not increase the difference between the effect on \( \varepsilon_T \) of changes in \( k \) and \( \varepsilon \).

For a smaller value of \( k \), the difference between Figs 8(b) and 3(b) is amplified, while for a larger value of \( k \), Fig. 8(b) becomes indistinguishable from Fig. 3(b)—compare the long dashed lines in Figs 4(c) and 9(b). This is as we would expect, that a very small perturbation in either the crack-normal or aspect ratio distributions from the perfectly aligned identical aspect ratio limit would be indistinguishable.
A change in $k$ is distinguishable from a change in $\varepsilon$, although only at higher frequencies (see Fig. 9b), where at low frequencies increasing $k$ to infinity appears equivalent to increasing $\varepsilon$ to 0.242 and decreasing $k$ to 1.0 is almost equivalent to decreasing $\varepsilon$ to 0.0034. The $P$-wave attenuation parameter $Q_{\gamma P}$, also shows similar behaviour for this model as it does for the variable aspect ratio model (see Fig. 10a). A change in the value of $P_m$ would alter this figure marginally for the smaller values of $P_m^\alpha$. The change in $Q_{\gamma P}$ with a change in $k$ or $\varepsilon$ is illustrated in Fig. 10(b). We note that while we see a close correspondence between increasing $k$ to infinity and increasing $\varepsilon$ to 0.023, and also between decreasing $k$ to 1.0 and decreasing $\varepsilon$ to 0.01, the values of $\varepsilon$ at which this correspondence occurs differ from those at which a similar correspondence occurs in $\varepsilon_r$ (see Fig. 9b). As with the variable aspect ratio model, the peak in $Q_{\gamma P}$ is seen to occur at the same frequency at which $\varepsilon_r$ has a maximum gradient.

A variation in the $SH$-wave attenuation coefficient, $Q_{\gamma SH}$, is seen with a variation in $P_m^\alpha$ (Fig. 11a). It is seen that for large enough values of $P_m^\alpha$, there is a second (small) peak in $Q_{\gamma SH}^{-1}$ parallel to the cracks. For $P_m^\alpha = 10^6$, such that a second peak occurs, the variation in $Q_{\gamma SH}$ with $k$ and $\varepsilon$ is given in Fig. 11(b). While we are able to match the height of the low-frequency peak resulting from a change in $k$ by a corresponding change in $\varepsilon$, the existence and relative height of the higher-frequency peak enables us to distinguish between the two competing effects.

For lower values of $P_m^\alpha$, at which this second, smaller peak does not occur, the effects of $k$ and $\varepsilon$ become indistinguishable. The peaks in $Q_{\gamma SH}$ occur at the frequency at which $\gamma_T$ has a maximum gradient, thus for smaller $P_m^\alpha$ when $\gamma_T$ exhibits only one region of change (see Fig. 8b), there is only the one peak in $Q_{\gamma SH}$, while for larger $P_m^\alpha$, $Q_{\gamma SH}$ exhibits a second peak.

9 DISCUSSION

We have seen that for both the variable aspect ratio and the variable orientation models there exist critical (non-dimensional) frequencies in both the variation of Thomsen’s parameters and the attenuation coefficients at which either a peak is reached or a transition is made from one value to another. The significance of these critical frequencies is their potential use in determining estimates of the unknown parameters within the model—$\varepsilon$, $\eta_0$, $\delta$, $k$, and $\tau$. $P_m^\alpha$ can be determined as the direction corresponding to maximum attenuation. We rely, then, on the value of $\varepsilon$ being such that the critical (non-dimensional) frequencies are attainable within the frequency range that can be achieved seismically ($1 < \omega < 10^4$ rad s$^{-1}$). Estimates of $\tau$ (Hudson et al.)
values of \( v_t \) on the range of values of attenuation coefficients. Our ability to do this depends not only on the variable orientation model alone, it appears that we ought to be able to both notice and differentiate between the effects of the variance of one or other of the models. Furthermore, we believe that there is some hope of distinguishing the effects of the variance of our model from those of the other.

Critically, however, there is a dependence upon the undetermined parameter corresponding to the relaxation time of pressure equalization between cracks, \( \tau \). Although estimates of this parameter have been made (Hudson et al. 1996; O’Connell & Budiansky 1977), a numerical investigation remains the subject of future work.

### 10 CONCLUSIONS

The model proposed by Hudson et al. (1996) for the transfer of fluid between connected cracks via non-compliant pores has been extended to allow for a continuous distribution of values of both crack orientation and aspect ratio. This more realistic model has the expected properties that at high frequencies the cracks behave as if isolated, while at low frequencies they behave as if undrained, and agree with the results of Brown & Korringa (1975). In the fully aligned limit they behave as if isolated at both high and low frequencies.

We looked separately at the cases of allowing the aspect ratio and orientation to vary, while keeping the other fixed, and studying the frequency dependence of Thomsen’s parameters and the attenuation coefficients. For both models, we considered whether or not we were able to notice, and differentiate between, the effects of the variance of the distribution and the crack density of the model. Furthermore, we addressed the issue of differentiating between the effects of the variable aspect ratio and orientation.

We believe that it is possible to both notice and differentiate between the effects of the crack density and the variance of one or other of the models. Furthermore, we believe that there is some hope of distinguishing the effects of the variance of one model from those of the other.

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### REFERENCES


\[ \dot{m}_n = \sum_m p_n^m M_n^m = p_0^m M_n^m + \sum_{m \neq n} p_n^m M_n^m. \]  

Fluid mass is preserved and does not concentrate in the pores, so

\[ \sum_m M_n^m = 0 \]  

(A3)

or

\[ \sum_{m \neq n} M_n^m = -M_n^m. \]  

(A4)

thus

\[ \dot{m}_n = -C \left[ p_0^m - \sum_{m \neq n} p_n^m M_n^m \right] / \sum_{m \neq n} M_n^m \right]. \]  

(A5)

where

\[ C = \sum_{m \neq n} M_n^m = -M_n^m. \]  

(A6)

We make the approximation

\[ \sum_{m \neq n} p_n^m M_n^m \approx p_0 \]  

since it is clearly a weighted average of the pressure in the cracks (excluding the nth) and the weights decrease with distance, becoming negligible (probably) at several crack spacing lengths. Then

\[ \dot{m}_n = -C \left[ p_0^m - p_0(x^0) \right], \]  

(A8)

where \( p_0(x^0) \) is an average of the \( p_0 \) over a region \( D_n \) centred on \( x^0 \), the centroid of the nth crack. Taking the average over \( D_n \),

\[ \tilde{\dot{m}}(x^0) = \frac{1}{D_n} \int_{x^0} \left[ p_0(x^0) - \sum_m w_m(x^0) p_0^m(x^0) \right] \sum_m w_m(x^0) \right]. \]  

(A9)

where \( w_m \) are weight functions. Thus,

\[ \tilde{\dot{m}}(x^0) = C \sum_m w_m(x^0) p_0(x^0) - p_0(x^0) \right] / \sum_m w_m(x^0) \right]. \]  

(A10)

We identify

\[ C = \frac{\phi}{\kappa \tau}, \]  

(A11)

a constant of appropriate dimensions, containing an unknown relaxation parameter, \( \tau \).

**APPENDIX B: THOMSEN’S PARAMETERS**

In the conventional condensed, two-subscript, 6 x 6 matrix notation, pairs of indices are represented as a single index: \( ij \rightarrow p, kl \rightarrow q \), such that 11 → 1, 22 → 2, 33 → 3, 23 → 4, 13 → 5 and 12 → 6. We thus use the representation \( C_{ijp} \) rather than \( c_{ijkl} \) (eq. 1).
We make use of the anisotropy parameters defined by Thomsen (1986) for vertically transversely isotropic material,

\[ \varepsilon_T \equiv \frac{C_{11} - C_{33}}{2C_{33}} , \]  

\[ \delta_T \equiv \frac{(C_{13} + 2C_{44}) - (C_{33} - C_{44})^2}{2C_{33}(C_{33} - C_{44})} , \]  

\[ \gamma_T \equiv \frac{C_{66} - C_{44}}{2C_{44}} , \]  

where the real part is assumed when the stiffnesses are complex.

We may use the wave speeds, eqs (C9) and (C10), to calculate two of these parameters,

\[ \varepsilon_T = \frac{v_g(90^\circ) - v_g(0^\circ)}{v_g(0^\circ)} \]  

and

\[ \gamma_T = \frac{v_g(90^\circ) - v_g(0^\circ)}{v_g(0^\circ)} , \]  

to first order in \( \varepsilon \).

**APPENDIX C: WAVE SPEEDS AND Q**

We make the assumption that the mean wave is a plane harmonic wave, \( \mathbf{u} = \mathbf{b} e^{k \cdot x} \) and substitute this into the time-harmonic equation of motion,

\[ \frac{\partial}{\partial x_p} \varepsilon_{pjq} \frac{\partial}{\partial x_q} + \rho \omega^2 u_i = 0 , \]  

where \( \rho \) is the density of the matrix and \( \omega \) the frequency of the propagating wave. We have

\[ \left[ \rho \omega^2 \delta_{ij} - \varepsilon_{pjq} k_p k_q \right] b_j = 0 . \]  

The attenuation coefficient \( Q^{-1} \) is given by

\[ Q^{-1} = 2 \left\| \frac{\mathbf{f}_m(k)}{\mathbf{R}_m(k)} \right\|^2 \]  

For a given \( \omega \), we let \( \mathbf{k} = \mathbf{k}^0 + i \mathbf{k}^1 \) and \( \mathbf{b} = \mathbf{b}^0 + i \mathbf{b}^1 \) and equate coefficients of \( i^0 \) and \( i^1 \) in eq. (C2). Thus, at \( \mathcal{C}(i^0) \) and \( \mathcal{C}(i^1) \) we have

\[ M_j b^0_j = 0 , \]  

\[ M_j b^1_j = N_j b^0_j , \]  

where

\[ M_j = \rho \omega^2 \delta_{ij} - \varepsilon_{pjq} k_p k_q , \]  

\[ N_j = \varepsilon_{pjq} (k_p k_q + k_j k^0_q) + \varepsilon_{pjq} k^0_j k^0_q . \]  

The \( \mathcal{C}(i^0) \) term is just the isotropic result. To first order, the cracks have normal \((0, 0, 1)^T\) and the rotational symmetry of the problem ensures that the material is transversely isotropic, so that, for a given \( \omega \), we can rotate the \((x_1, x_2)\) plane such that

\[ \mathbf{k}^0 = \frac{\omega}{v} \sin(\theta, 0, \cos(\theta))^T \]  

for some incident angle \( \theta \), where \( v = v_P \) or \( v_S \), corresponding to quasi-\( P(\mathbf{q}P) \) waves, or quasi-\( S(\mathbf{q}S) \) waves, respectively. For the \( \mathbf{q}P \) wave, we have \( b^0_{qP} = (\sin(\theta, 0, \cos(\theta))^T \), while for the \( \mathbf{q}S \) waves we have \( b^0_{qS} = (\cos(\theta, 0, -\sin(\theta)) \), corresponding to \( \mathbf{q}SV \) and \( \mathbf{q}SH \) waves, and we are free to choose the magnitude of \( \mathbf{b}^0 \). Pre-multiplication of the \( \mathcal{C}(i^0) \) term with \( \mathbf{b}^0 \) yields a single equation for the components of \( \mathbf{k}^1 \),

\[ b^0_j N_j b^0_j = 0 . \]  

On the assumption that \( \mathbf{k}^1 \) is parallel to \( \mathbf{k}^0 \), this becomes an expression for the magnitude of \( \mathbf{k}^1 \).

The wave speeds, to first order, are given by

\[ \frac{v_{gP}}{v_P} = 1 + \frac{\varepsilon}{2(\lambda + 2\mu)} \times \mathbf{R}_m \left( \sin^2(\theta) C^1_{33} + \cos^2(\theta) C^1_{33} + \frac{1}{2} \sin^2(\theta) C^1_{13} + \sin^2(\theta) C^1_{55} \right) . \]  

\[ \frac{v_{gSH}}{v_S} = 1 + \frac{\varepsilon}{2\mu} \mathbf{R}_m \left( \cos(\theta) C^1_{44} + \sin^2(\theta) C^1_{66} \right) . \]  

These are equivalent to Hudson (1981).

From eq. (C3), the attenuation coefficient is given by

\[ Q^{-1} = \frac{2\varepsilon}{\omega} \left\| \mathbf{f}_m(k^1) \right\|^2 \]  

to first order for \( v = v_P \) or \( v_S \) and the appropriate \( k^1 \). Thus,

\[ Q_{qP}^{-1} = \frac{\varepsilon}{\lambda + 2\mu} \left\| \mathbf{f}_m \left( \sin^2(\theta) C^1_{11} + \cos^2(\theta) C^1_{11} + \frac{1}{2} \sin^2(\theta) C^1_{13} + \sin^2(\theta) C^1_{55} \right) \right\| , \]  

\[ Q_{qSV}^{-1} = \frac{\varepsilon}{\mu} \left\| \mathbf{f}_m \left( \frac{1}{4} \sin^2(\theta) C^1_{11} + C^1_{13} - 2C^1_{11} + \cos^2(\theta) C^1_{55} \right) \right\| , \]  

\[ Q_{qSH}^{-1} = \frac{\varepsilon}{\mu} \left\| \mathbf{f}_m \left( \cos^2(\theta) C^1_{44} + \sin^2(\theta) C^1_{66} \right) \right\| . \]  

**APPENDIX D: NON-ZERO CONTRIBUTING TERMS OF \( \Omega \)**

We start by defining the integral

\[ I_{m,n} = b(k) \int_0^{\pi/2} \sin^m\theta \cos^n\theta e^{\pm i \omega t} d\theta . \]  

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The components of $\Omega_{\delta \delta \delta \delta}$ that contribute to $T_{\kappa \kappa \nu}$ (eq. 74) are

\[
\begin{align*}
(\Omega_{11111} + \Omega_{21121}) &= \frac{3}{8} I_{0.2} + \frac{1}{8} I_{3.0} = (\Omega_{1212} + \Omega_{22222}), \quad (D2) \\
(\Omega_{1212} + \Omega_{21221}) &= \frac{1}{8} I_{0.2} + \frac{3}{8} I_{3.0} = (\Omega_{1212} + \Omega_{22222}), \quad (D3) \\
(\Omega_{13131} + \Omega_{23131}) &= \frac{1}{2} I_{1.4} + \frac{1}{2} I_{1.2} = (\Omega_{1212} + \Omega_{22222}), \quad (D4) \\
(\Omega_{11112} + \Omega_{21122}) &= -\frac{1}{8} I_{3.0} = -\Omega_{11132}, \quad (D5) \\
(\Omega_{11133} + \Omega_{21223}) &= -\frac{1}{2} I_{3.2} = (\Omega_{12213} + \Omega_{22223}) = -\Omega_{11313} \\
&= -\Omega_{22233}, \quad (D6) \\
(\Omega_{13133} + \Omega_{23133}) &= I_{3.2}, \quad (D7) \\
\Omega_{31331} &= \frac{3}{8} I_{5.0} = \Omega_{32332}, \quad (D8) \\
\Omega_{32332} &= \frac{1}{8} I_{0.0} = \Omega_{32131}, \quad (D9) \\
\Omega_{53333} &= \frac{1}{2} I_{3.2} = \Omega_{32332} = \Omega_{31331} = \Omega_{32332}, \quad (D10) \\
\Omega_{33333} &= I_{3.4}, \quad (D11) \\
\end{align*}
\]

and those related to the above by the symmetries

\[
\Omega_{\delta \delta \delta \delta} = \Omega_{\delta \delta \delta \delta}, \quad \Omega_{\delta \kappa \kappa \kappa} = \Omega_{\delta \kappa \kappa \kappa}.
\]

**APPENDIX E: VARIABLE ASPECT RATIO AND ORIENTATION**

For completeness, we give an expression for the first-order correction to the elastic constants derived by allowing both the aspect ratio and the orientation to vary while remaining independent of one another:

\[
\begin{align*}
c_{1_{ij}} &= -\frac{1}{\mu} \frac{\phi_{ij}}{\phi_{0}} T_{\kappa \kappa \nu}, \quad (E1)
\end{align*}
\]

where

\[
T_{\kappa \kappa \nu} = \left( \delta_{11} \delta_{11} + \delta_{12} \delta_{12} \right) \tilde{W}_{11} + \frac{8}{3} \delta_{33} \delta_{13} (1 - v) \left( \frac{1 - \nu \tau}{1 - \nu \tau} \right) \Omega_{\delta \delta \delta \delta} \left[ \frac{8}{3} (1 - v) \Pi_{\theta} \Pi_{\alpha} \left( \gamma_{0} - 1 \right) F_{1} - \frac{K_{1}}{K} (F_{2} - F_{1}) \right] \frac{F_{1}}{1 - \nu \tau} \\
&\times \left[ \gamma_{0} F_{1} + \left( 1 - \frac{K_{1}}{K} \right) (F_{2} - F_{1}) + i \tau P (1 - \nu \tau) \right]^{-1}.
\]

\[(E2)\]